

Three Phase Multilevel Shunt Active Power Filters With Non Linear Loads for power quality Improvement

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Abstract

This work presents a three phase shunt active power filter based inverter with Multi Levels. In this study, the novel approach i.e NPC based Multi-Level inverter proposed. The proposed approach reveals unwanted active current component with fundamental frequency contained in the compensation current which causes oscillation and fall of the DC voltage level of shunt active power filter. The proportional-integral controller that has been widely used by researchers is used to maintain the reference DC voltage level. The proposed system is modeled with MATLAB/Simulink and simulation studies are carried out on RL and RC type load with both PI controller and Fuzzy controller. The obtained results from the simulation studies show that the proposed

approach give the good results when the level of the inverter increases.

Key Words: NPC; Multilevel; PI; Fuzzy;.

1 Introduction

Increased use of power electronics appliances in industrial, commercial and domestic applications results in rapid variation of reactive power and augmented deterioration of the power systems voltage and current waveforms [1]. The introduction of harmonics in the utility system leads to greater power losses in distribution networks, overloading, overheating and failure of power factor correction capacitors [2]. These systems are more prone to power quality issues as they include microelectronic control systems, which work with very low energy levels [3]. There are several consequences of distortion of the supply network such as

- Harmonic level augmentation resulting from series and parallel resonance.
- Spurious operation of fuses, circuit breakers and protective equipments.
- Reduced product and reduced quality assurance to consumers.

Owing to these problems, the issue of power quality delivered to the end customers is becoming a thing of serious concern. International standards concerning electrical power quality such as IEEE-519, IEC 61000, EN 50160 put forth that electrical equipments and facilities should not produce harmonic currents greater than the specified values and also specify the distortion limits to the supply voltage [4]. Traditionally shunt passive filters, which consists of tuned LC filters are employed to improve power factor and to suppress unwanted harmonics in power systems. Principally, the impedance ratio of the source and the shunt passive filter determines the filtering characteristics of passive filter [5]. As a result, there are certain factors which discourage the use of passive filters such as

- The shunt passive filter which acts as a sink to the harmonic current flowing from the source falls in series resonance with the source impedance .
- Harmonic amplification at specific frequency.
- Component ageing

- Fixed compensation for specific loads.

To overcome the above disadvantages, currently Active Power Filters (APFs) are identified as an appropriate solution for power quality problems.

There are several topologies of active power filters for harmonic mitigation such as series, shunt, series-shunt type (unified power quality conditioner) and hybrid configurations [6]. The series active power filters are employed for voltage harmonic compensation. The necessity of current harmonic compensation in many industrial applications paved the popularity of shunt APFs than series active filters. Among various power circuit topologies for SAPF, Voltage Source

Inverters (VSI) is an attractive solution to harmonic current problems. Due to the power handling capabilities of power semiconductors, these two-level inverters are limited for low power applications [7]. The harmonic reduction in output waveform without increasing switching frequency or decreasing the inverter power output makes Multi Level Inverters (MLIs) as an ideal suggestion for the power circuit topology of SAPF [8]. With increase in the number of levels, the output voltages of the MLIs have more steps in synthesizing a nearly sinusoidal waveform, thereby reducing harmonic distortion [9]. A multilevel inverter with m -levels, can increase the capacity by $(m-1)$ times than that of two-level inverters through the series connection of power semiconductor devices without additional circuit to have uniform voltage sharing [10]. There are three well known topologies of MLIs [11] : Neutral Point Clamped (NPC) MLI, the Flying Capacitor (FC) MLI and the Cascaded H-Bridge MLI (CHBMLI). The first generation of MLI called NPC multi-level inverter, also called diode-clamped, was introduced by Nabae et al [12] which was a three-level inverter. Both NPC and FC MLIs makes use of redundant switching states for the regulation of dc voltage [13].

However, the number of diodes and capacitors increases with increasing the number of voltage levels leading to complicated control scheme. Cascaded MLIs are preferred for harmonic mitigation without having voltage unbalance problem and there are no extra clamping diodes or voltage balancing capacitors [14]. In this work, 5-level CHBMLI has been used as the shunt active power filter for harmonic suppression.

To put shunt APF in effective use, it is essential to adopt a suitable control strategy for the extraction of reference compensation currents. Instantaneous active and reactive power theory (p-q theory), unity power factor method, one cycle control, Fast Fourier Techniques (FFT), Fryze power theory are some of the control strategies for reference current extraction in active power filters as given in the literature. H.Akagi put forth p-q theory which is quite efficient method for balanced three phase loads, but this method requires a number of calculations, complex mathematical transformations and suffers from synchronization problems [1]. In 1995, Bhattacharya proposed the calculation of d-q components called Synchronous Reference Frame (SRF) theory which is concise and yields good dynamic performance [15].

The energy loss due to conduction and switching power losses associated with the diodes and MOSFETs of the inverter in APF tend to reduce the value of dc voltage across the dc capacitor. Thus, the maintenance of constant dc voltage across the capacitor connected to the inverter is another important aspect to be considered in the development of active filters. In this work, SRF theory which incorporates PI controller for dc voltage regulation of SAPF is used as an efficient control strategy for reference current extraction of the SAPF. Various PWM current control strategies for shunt active power filter have been proposed in literature [16]. In this work, the switching pulses for the cascaded inverter switches are generated using Triangular-Carrier Current controller (TCC). This paper is organized in five divisions. Commencing with an introduction, the subsequent sections cover configuration of SAPF, the control strategies for SAPF, simulation results of the proposed system and the concluding remarks.

2 SHUNT ACTIVE FILTER CONFIGURATION

2.1 Compensation Principle

The shunt active power filter behaves as a current source injecting the harmonic components generated by the load which are equal but phase shifted by 180° , which forms the basic principle of SAPF. As a

result, components of harmonic currents in the load are cancelled by the effect of shunt active power filter and the source current remains sinusoidal and in phase with the respective voltage. The complete diagrammatic representation of CHBMLI based shunt active power filter is shown in Fig.1. The three phase source is connected to diode rectifier (non-linear) load. The SAPF is realized with 5-level CHBMLI consisting of 24 MOSFETs/Diodes, a dc-side capacitor and RL filter (RF, LF) which suppresses the harmonics caused by the switching operation of the MOSFET inverter.

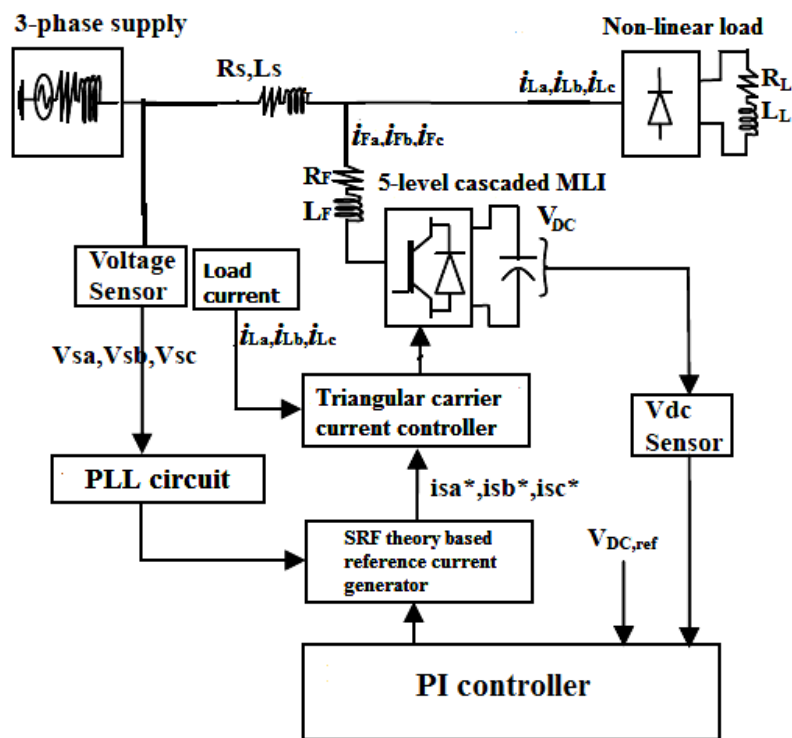


Fig.1 Principle of proposed SAPF system

The control scheme consists of PI for DC voltage regulation, SRF theory for reference current generation and the TCC to spawn the switching pulses for driving switches in the MLI.

2.2 5-level Cascaded H-Bridge Multilevel Inverter (CHBMLI)

A 3-phase, 5-level Cascaded H-Bridge Multilevel Inverter (CHBMLI) depicted in Fig.2 is used as the power circuit for shunt active power filter in this work. This inverter requires two, two-leg, series connected H-bridges and four triangular carrier waves [17]. Fig.2 shows two H-bridges connected to a single phase consisting of two parallel legs which has two MOSFETs as a switching device, in a single leg. For a 5-level MLI, $m=5$, where m is the number of levels in MLI, four carrier waves are required. The output of the current controller are applied as gating pulses for the inverter switches. The triangular carrier current controller is put in use as it has uniform switching stress for each phase. The MLI has two series connected H-bridges per phase with V_{dci1} and V_{dci2} as two voltages to be regulated, where i corresponds to the three phases (a,b,c) of the inverter. The number of output voltage levels of CHBMLI is given by $2n+1$, where n is the number of H-bridges connected in cascade.

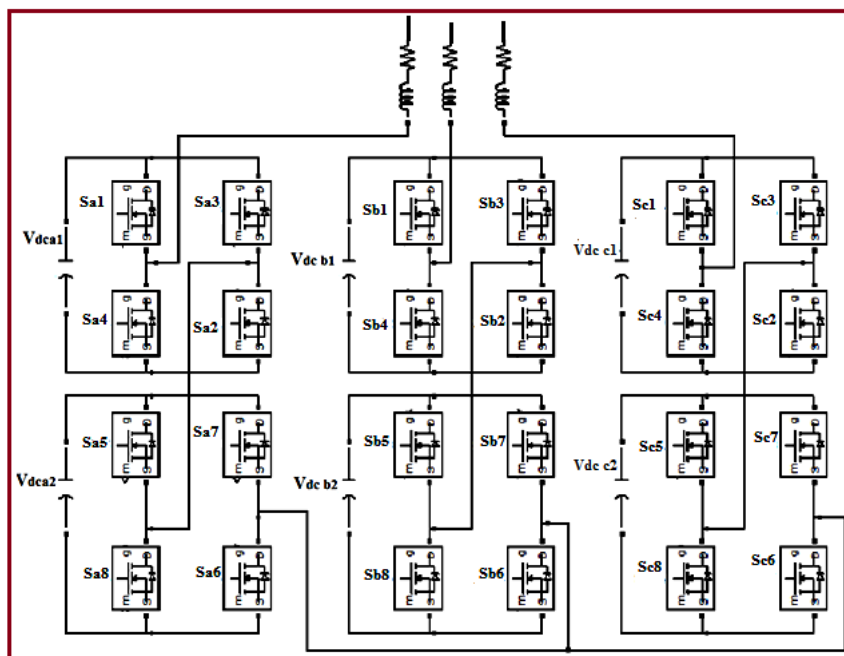


Fig.2. 5-level, Cascaded H-Bridge Multilevel Inverter

3 CONTROL STRATEGIES

3.1 Reference current extraction

In this work, the time domain based synchronous reference frame theory is utilized to extract the reference current from the distorted line current. Fig.3 shows the basic block diagram of SRF theory consisting of PLL circuit for the generation of unit vectors ($\sin \theta$ and $\cos \theta$) and a controller for dc-side capacitor voltage regulation.

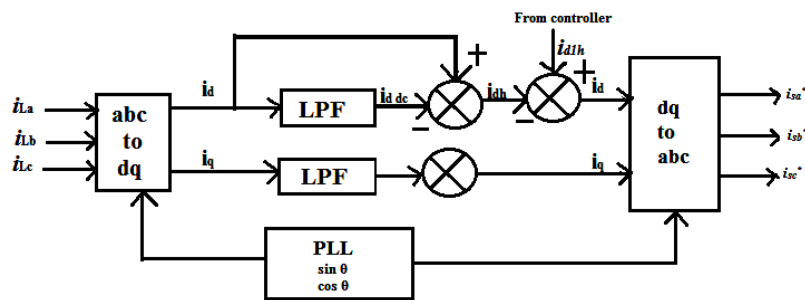


Fig. 3. Block diagram of SRF theory

In this method, the three phase load currents i_{La} , i_{Lb} , i_{Lc} are first detected and transformed into two-phase synchronous (or rotating) frame (d-q axes) using parks transformation as given in Eqn.1.

$$\begin{pmatrix} i_d \\ i_q \end{pmatrix} \tag{1}$$

The reference frame is rotating synchronously with fundamental currents. This results in time variant currents with fundamental frequencies which are constant after

$$\frac{2}{3} \begin{pmatrix} \sin \theta & \sin \theta - \frac{2\phi}{3} & \sin \theta + \frac{2\phi}{3} \\ \cos \theta & \cos \theta - \frac{2\phi}{3} & \cos \theta + \frac{2\phi}{3} \end{pmatrix}$$

transformation. Each current component (i_d , i_q) has an average value or dc component and an oscillating value or ac component as shown in Eqn.2.

$$i_d = \bar{i}_d + \tilde{i}_d i_q = \bar{i}_q + \tilde{i}_q \quad (2)$$

The i_d and i_q currents obtained from park transformation are passed through a Butterworth type low pass filter to eliminate dc components in the non-linear load currents. To minimize the inverter losses, the required current is added to the positive sequence fundamental frequency active component of the d-q current [18]. Now the currents from two phase synchronous frame are transformed back into three-phase stationary (a-b-c) frame using inverse Parks transformation as per Eqn.3 and the required reference currents are obtained.

$$\begin{bmatrix} i_{sa}^* \\ i_{sb}^* \\ i_{sc}^* \end{bmatrix} = \begin{bmatrix} \sin\theta & \cos\theta \\ \sin\theta - \frac{2\phi}{3} & \cos\theta - \frac{2\phi}{3} \\ \sin\theta + \frac{2\phi}{3} & \cos\theta + \frac{2\phi}{3} \end{bmatrix} \begin{pmatrix} i_d \\ i_q \end{pmatrix} \quad (3)$$

The obtained reference signals (i_{sa}^* , i_{sb}^* , i_{sc}^*) are compared with the actual load currents in a comparator and the output which acts as the reference signal for triangular carrier current controller. This consequently provides gating signals to trigger the switches of the MLI.

3.2 DC link voltage regulation

For the APF to work properly, it is essential that the capacitor voltage at the dc-link must remain constant. For this purpose the active power flowing into the active filter needs to be monitored. The dc-link voltage can be maintained at the desired value, if the active power flowing into the filter can be controlled equal to the losses inside the filter. In view of practical implementation, dc-link voltage fluctuations may result from commutation, conductance and own-capacitor losses plus control system delays. The filter operates as a controlled rectifier thereby transferring a little amount of active power from the ac to the dc side of the inverter, for compensating the voltage variations. In order to maintain dc link voltage constant and to generate the compensating reference currents, PI controller is used in this work.

3.3 Fuzzy controller intended for dc link voltage regulation

The dc-side capacitor voltage is sensed and compared with a set reference voltage. The Fuzzy controller which promotes to zero steady state error in tracking the reference current signal, processes the comparison result of the voltage error given by $e = V_{dc-ref} - V_{dc}$. The output of the Fuzzy controller (i_{d1h}) represents the total active current required to maintain V_{dc} at a constant value which in turn compensates for the power losses.

3.4 Triangular carrier current controller

Most of the current control techniques used for APF are based on PWM-current control strategy. However, the high performance of the current-control is a difficult task in most practical cases, where the inverter load is unidentified and changeable. For the efficient performance of the SAPF, it is essential that the system must supply current in response to the generated reference current. In this work, triangular carrier current controller has been used for the generation of current pulses for the switches of CHBMLI. The reference currents are compared with the actual load currents. This error current is used as the modulating signal and is compared with the four carrier signals in the TCC to produce necessary gating signals for the inverter switches. Fig. 4 shows the current control scheme using TCC for phase a of the CHBMLI.

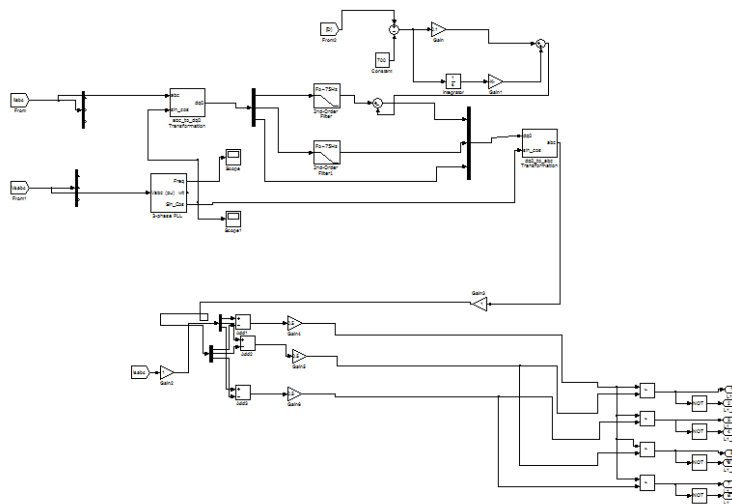


Fig. 4. Current pulse generation for phase a using TCC

4 SIMULATION RESULTS

The proposed technique is implemented in MATLAB/SIMULINK working platform to validate the performance of the system using PI controller. The effectiveness of PI controller is proved in terms of THD minimization of source currents before and after compensation. The simulation time is taken as 50 s and the proposed system is simulated for 0.5s. Here, three phase diode rectifier with RL/RC load is taken as the non-linear load.

4.1 Simulation results for uncompensated system

Fig.5 shows the source current waveforms before compensation with the SAPF. The corresponding harmonic spectrum is shown in Fig. 6.

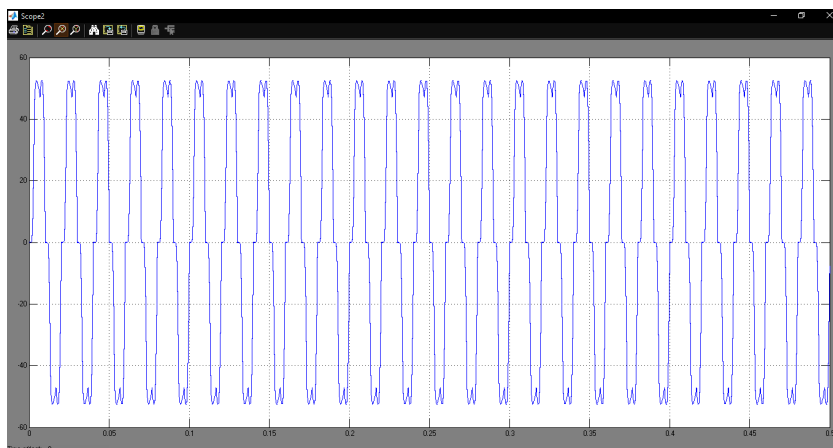


Fig. 5 Source current before Compensation

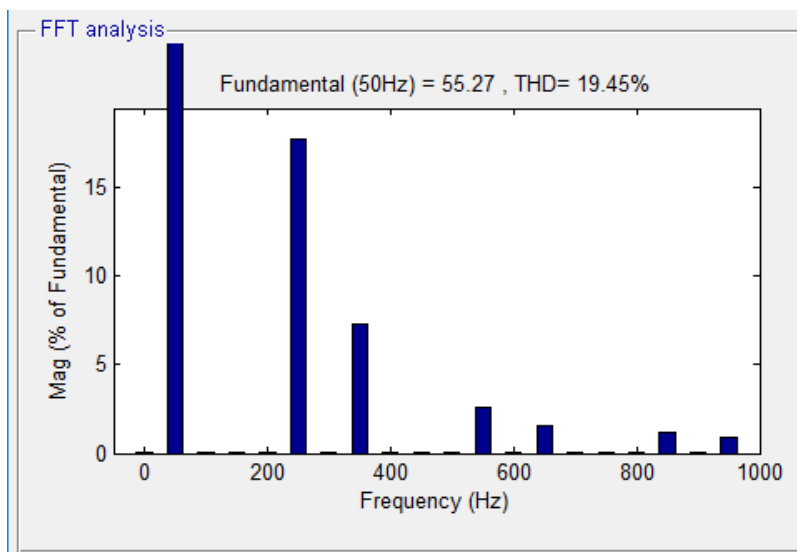


Fig. 6 Source current spectrum for uncompensated system

4.2 Simulation results with PI controller

The control circuit in SIMULINK model uses SRF theory for reference current generation, TCC for triggering pulse generation and PI controller for dc voltage regulation. The system parameters for

simulation are given in Table I. shows The simulation model of SAPF system with PI controller is shown in. Fig.7 The simulated waveforms of source current and injected current after APF application with PI controller are given in Figs. 8 and 9 respectively. The harmonic spectrum of the source current after compensation with PI controller is shown in Fig

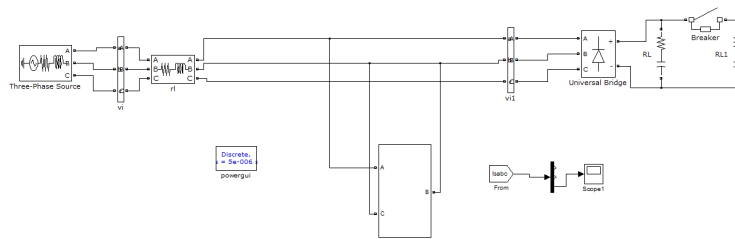


Fig. 7 Simulation model of SAPF system with PI controller

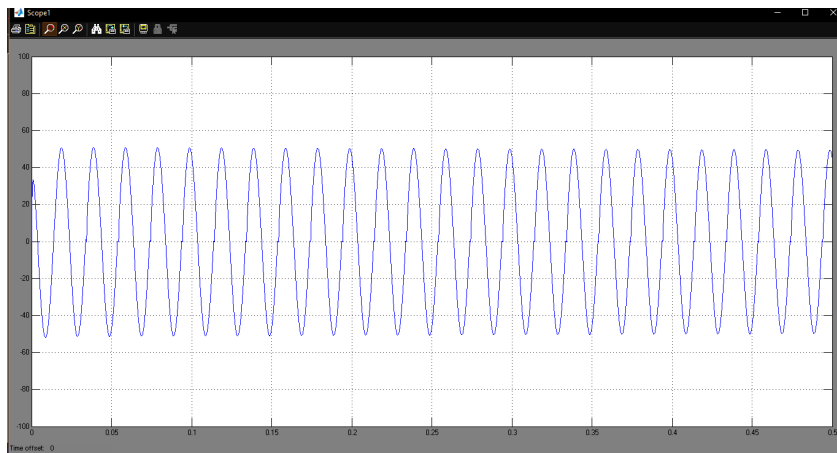


Fig.8 Source current after compensation with PI controller

Time interval (s)	Load condition	Source current THD with PI controller (%)	
		RL Load	RC Load
0.05-0.2	Initial load	3.15	3.39
0.2-0.3	Increase in load	3.61	4.84
0.3-0.5	Decrease in load	2.60	3.05

TABLE I HARMONIC PERFORMANCE OF SIMULATION FOR RL/RC LOAD

4.3 Simulation results with Fuzzy controller:

The control circuit in SIMULINK model uses SRF theory for reference current generation, TCC for triggering pulse generation and Fuzzy controller for dc voltage regulation. The simulated waveforms of source current after APF application with Fuzzy controller are given in Figs. 9. The harmonic spectrum of the source current after compensation with Fuzzy controller is shown in Table II.

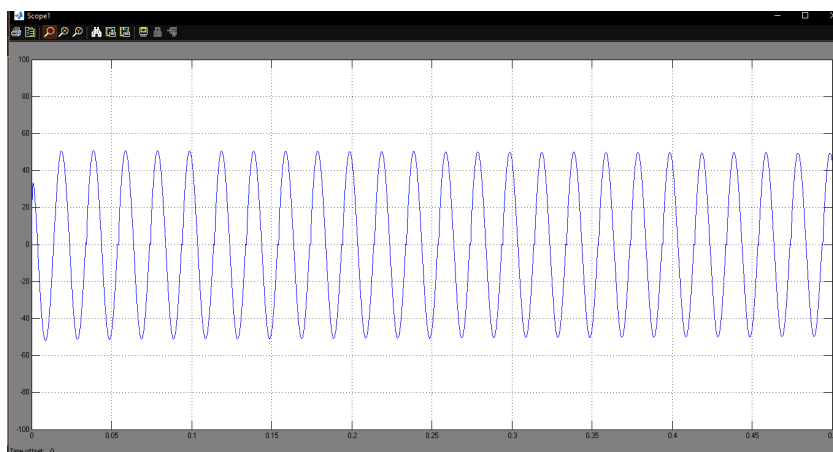


Fig.9 Source current after compensation with Fuzzy controller

Time interval (s)	Load condition	Source current THD with Fuzzy controller (%)	
		RL Load	RC Load
0.05-0.2	Initial load	2.06	0.53
0.2-0.3	Increase in load	1.49	0.68
0.3-0.5	Decrease in load	1.49	0.97

TABLE II HARMONIC PERFORMANCE OF SIMULATION FOR RL/RC LOAD

5 CONCLUSION

In this paper, a three level and five-level multilevel inverter based SAPF incorporating PI and Fuzzy control for dc voltage regulation is presented. The purpose of this filter is to eliminate the harmonics imposed by non-linear loads. To validate the performance of the proposed system extensive simulations are performed on MATLAB/Simulink platform using diode bridge rectifier with RL/RC load. The simulation results justifies the robustness and effectiveness of the SAPF system with PI controller under varying load conditions and unbalanced source voltage. The THD of source current is significantly reduced from 29.89% to 0.48 % with the utilization of PI and Fuzzy controller. The control strategy for reference current extraction based on Synchronous Reference Frame theory provides a better extraction of reference compensation currents from the distorted line current. Thus it is ensured that the proposed SAPF system renders appreciable performance to control shunt active filters based on multilevel inverter topology towards the mitigation of harmonics.

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