

Balanced radial distribution system dynamic phasor modeling using PVA

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Abstract

With the expansion in entrance of sustainable sources in distribution system, the control methods are likewise advanced from recent years. In this paper we consider an unbalance spiral distribution system with PVA (Photo Voltaic Array) interconnected to the distribution system through VSI (Voltage Source Converter). The controller produces beats through sinusoidal PWM (Pulse Width Modulation) system fed to VSI with matrix voltage synchronization control. The PI controller in the system is supplanted with fluffy controller to expand the reaction time of the VSI and diminish the THD in the network. The total investigation is completed in MATLAB Simulink programming with all graphical portrayal and logical charts rating of the lattice and VSI associated PVA.

1 Introduction

Keeping in mind the end goal to interconnect the inexhaustible sources (PVA) to the framework system a transformation is required

to change over the DC to three stage AC. The three stage AC must be in synchronization with the lattice in parameters of voltage, recurrence and stage. The VSI (Voltage source Inverter) is a three legged six IGBT switch inverter, where the DC side is associated with PVA and the three stage AC side associated with the matrix through LC channel. The LC sift is associated with soggy through the produced music shape the VSI keeping away from the music into the framework.

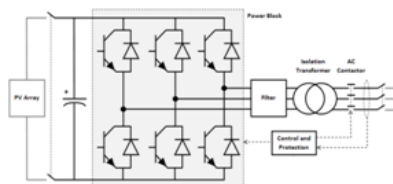


Fig. 1: VSI connected to grid using RES

Any interruption in the exchanging of the VSI while associated with the framework system may likewise disturb the network voltage expanding the powerlessness of gear associated with the system. It is extremely obligatory to keep up the exchanging of the VSI with ideal control systems. The controller detects the voltages and currents at the source side and furthermore the load side producing reference esteems for the age of heartbeats to VSI. The matrix system contain direct and non-straight loads, the impact of non-straight loads is higher than the direct loads. As the non-direct load takes a shot at DC an AC to DC converter is utilized with the assistance of power electronic switches. Load is just inductors or resistors, we don't have any capacitor loads. The aggregate impedance of the load associated with the AC to DC converter presenting music in the system making an extreme issue of PQ adjusting. These load current music caused by the power electronic gadgets can be remunerated through the APF (Active Power Filter) with RES by infusing required dynamic and receptive power. The pay lessens underline on fundamental source expanding the power factor and enhancing the power quality. The operational cost of the APF is less as RES is interconnected for the pay to the lattice.

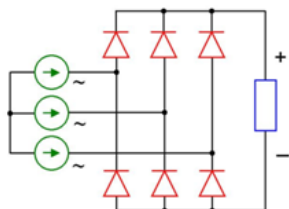


Fig. 2: Rectifier of non-linear load

The principle point of lattice system is to join the inexhaustible sources into the network with most extreme infiltration and to supplant the regular sources with the sustainable sources. The VSI ought to be controlled viably utilizing ideal control strategies with less conduction misfortunes to use the power from the inexhaustible sources and infuse dynamic power, with responsive power pay and decrease of music in the lattice system. The load stream can be controlled by controlling the tweak list of the key reference waveform of the VSI.

Because of this high utilization if receptive power from the source the power factor of the system drops to a low esteem ie., between 0.5 and 0.8. Because of the drop in the power factor the source presents music in the transmission line where the sounds are appropriated to the next distribution lines actuating the music into different loads which is caused by the modern load. It is essential to keep up the power factor of the distribution line and furthermore to diminish the THD caused by the other basic loads. A basic phasor chart with impedance load is demonstrated as follows.

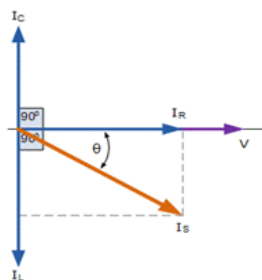


Fig. 3: Phasor diagram of impedance load.

The ordinary (d-axis) is considered as the reference phasor or the point of the supply voltage (V) accepting the edge as 0deg.

The phasor IR is the protection current which is in stage with the voltage and the relative edge between the voltage and the current IR is 0deg. There is additionally a fanciful axis (q-axis) with positive and negative vectors, where the positive vector is capacitor current (IC) and negative vector is considered as inductor current (IL). The two vectors are 90deg stage moved from the voltage vector with driving and slacking points as capacitive and inductive currents separately. At the point when the load edge is 0deg the power factor is ascertained as $\text{Cos}()$ which is '1' called as solidarity power factor. Solidarity power factor is the perfect power factor where the obvious power is same as that of the dynamic power and furthermore never accomplished. Presently, with the capacitive current (IC) the point is 90deg driving where the power factor with the above give condition is '0' zero power factor driving and the inductive current (IL) with 90deg slacking is ascertained as '0' zero power factor slacking.

The resultant current (IS) with an impedance load which incorporates resistive and inductive components has a point of '' in respect to the voltage (V) vector and the current (IS) vector. The power factor lessens step by step when the 'q-axis' part vector increment ie., inductive load increments. It is extremely basic to keep up the power factor in a scope of '0.9-1' in order to keep up the power quality. With a specific end goal to repay the edge between the voltage and the load current vector a capacitive loads must be included into the system. The capacitive loads has a '+q-axis' vector which remunerates the 'q-axis' part vector lessening the edge between the voltage vector and load current vector. The pay load phasor graph is appeared in fig. 5.

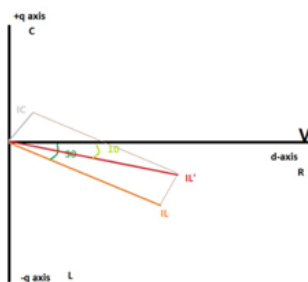


Fig. 4: Compensation phasor diagram

Where,

V= Voltage vector

IL = load current vector

IC = capacitor current

IL= resultant load vector

As we can obviously find in the above figure the edge between the voltage reference vector and the load is 30 deg ascertaining the power factor as 0.866. A repaying current (IC) is presented by including a capacitor load decreasing the relative point between the load vector from the voltage vector to 10deg expanding the power factor to 0.98.

Adding to the above load issues we likewise have hang and swell of voltage issues where swell is viewed as most basic issue in the whole electrical designing. Droops may not make prompt harm the system but rather it causes insipient harm to the gear. Swells are caused when extensive loads in the scope of uber watts are all of a sudden disengaged from the distribution system. It can be expounded as when the distribution system is sustaining substantial loads high currents stream in the lines, yet when this vast load is separated the utilization current is decreased instantly in the line. Keeping in mind the end goal to keep up the clear power in the distribution line the voltage increments abruptly making a voltage swell in the system. This impact is called Ferranti impact. The expanded voltage might be 125-150% to the ostensible voltage esteem which can be disposed of with either circuit breakers or FACTs gadgets, for example, DVR or UPQC.

Then again the lists are made when a huge load is all of a sudden associated with the distribution system. Because of the sudden including of substantial load the current in the line is expanded abruptly and as we talked about above to keep up the obvious power the voltage now will be diminished and droop is made. The system is said to be in droop when the voltage level goes underneath 95% of the ostensible esteem.

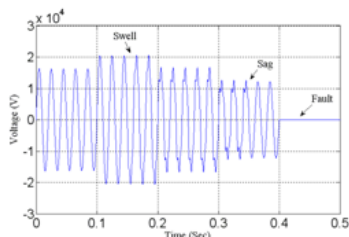


Fig. 6: Voltage profile with sag, swell & harmonics

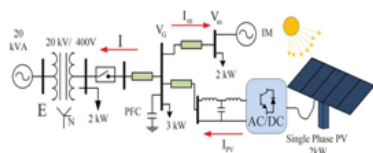


Fig. 5: Test system

The parameters displayed in [17] and [19] are used for the proposed think about system appeared in Fig. 1. The dispersed system comprises of a solitary stage PV station introduced in stage the system, a 3-stage induction machine, a 3-stage PFC, and a 3-stage load. Since the single-stage PV will present unbalance in the distribution system, the induction machine will be displayed to incorporate unbalance impact. Negative-arrangement segments in the stator voltage can cause a clockwise turning stator ux. At the point when this ux is interfacing with the counter-clockwise turning rotor ux, a 120-Hz torque swell will show up. Thusly, the turning velocity will have swells with 120-Hz recurrence. To tally in the negative impact, the dynamic model of a three-stage induction machine in [9] in view of succession segments is embraced in this paper. The space-vector model of a squirrel-confine induction machine with attractive immersion and opening music disregarded is displayed as takes after:

2 Modeling of PVA:

For effective inexhaustible power age PVA is utilized to create power from sun powered illumination. As the load request is expanding step by step the power age additionally must be expanded, yet

because of the customary method for power age is causing an Earth-wide temperature boost. Because of this the productivity of the PVA must be expanded by including silicon surface the board. And furthermore utilize MPPT systems to track greatest power amid any illumination and air conditions. The outline of PVA is done in MATLAB with Simulink obstruct, with numerical portrayal.

Voltage of PVA totally relies upon sun oriented illumination (Sx) and encompassing temperature (Tx). PVA (Photo voltaic cluster) is a mix of arrangement and parallel sun based cells orchestrated in an exhibit to produced the required voltage and current. Every arrangement blend of cells can be considered as photograph voltaic module. Increment in arrangement cells expands the voltage and increment in parallel cells builds the current limit. Plan for voltage of every cell is given beneath

$$V_c = \frac{AkT_c}{e} \ln\left(\frac{I_{ph} + I_0 - I_c}{I_0}\right) - R_s T_c$$

Where, k = Boltzmann constant (1.38×10^{-23} J/oK).

I_c = cell output current, Amp.

I_{ph} = photocurrent

I_0 = reverse saturation current of diode

R_s = series resistance of cell

T_c = reference cell operating temperature

V_c = cell voltage, V.

The Boltzmann constant and the reference temperature must be in same units ie., either 0C or 0K. The scientific displaying of the above condition can be developed utilizing simulink pieces is as underneath.

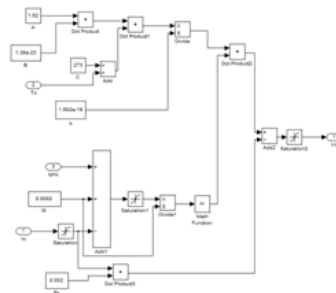


Fig. 6: Simulink model of Vc

The above outline is for a solitary cell voltage, so as to expand the voltage of the PVA the phone voltage must be increased to a coveted esteem considering every phone voltage as 0.4V. Thus, the quantity of arrangement associated cells (N_s) can be figured as

$$N_s = \frac{V_0}{4}$$

To get each cell current, the total current output from the dependable source has to be divided by number of parallel connected cells(N_p). Therefore, parallel connected cells are considered as

$$N_p = \frac{I_0}{I_{cell}}$$

The representation in simulink is taken as

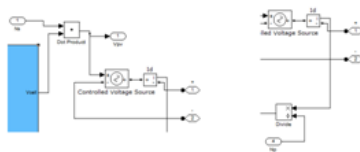


Fig. 7: Simulink modeling of N_s & N_p

For the calculation of V_{cx} (cell voltage) and I_{phx} (Photocurrent) we need correction factors C_{TV} C_{TI} C_{SV} C_{SI} . The formulation is given as

$$V_{CX} = C_{TV}C_{SV}V_C$$

$$I_{phx} = C_{TI}C_{SI}I_{ph}$$

The correction factors are given as

$$C_{TV} = 1 + \beta_T(T_a - T_x)$$

$$C_{TI} = 1 + \frac{\gamma_T}{S_C}(T_x - T_a)$$

$$C_{SV} = 1 + \beta_T\alpha_s(S_x - S_c)$$

$$C_{SI} = 1 + \frac{1}{S_c}(S_x - S_c)$$

Where, $\beta_T = 0.004$ and $\gamma_T = 0.06$
 T_a = reference temperature

T_x = ambient temperature
 S_c = reference solar irradiation
 S_x = ambient solar irradiation

The estimations of T_x and S_x changes relying on the Sun beams which change ceaselessly and capriciously. The impact of progress in sunlight based illumination fluctuates the cell photocurrent and furthermore the cell voltage (V_c). Give us a chance to consider the underlying sun powered illumination is I_{sx1} and the expansion of the light is I_{sx2} which thus expands the temperature from T_{x1} to T_{x2} , photocurrent from I_{phx1} to I_{phx2} . The numerical displaying of the amendment factors in simulink is given underneath

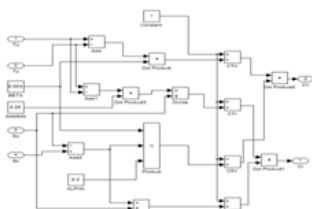


Fig. 8: CI & CV modelling

Depending upon the solar irradiation and temperature the values of CV & CI are calculated which is fed to V_c block to get the cell voltage value as shown below

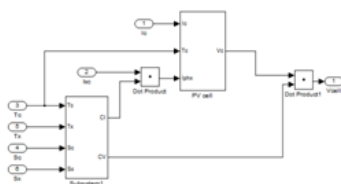


Fig. 18: Combined diagram of CV CI & Vc mathematical models

The aggregate system graph of the PVA with all the scientific plan are put into a subsystem to make it clear and reasonable. The yield of the V_c increased with the N_s consistent piece characterizing the aggregate voltage of the joined cells of the PVA is fed to the voltage controlled voltage source square in order to produce the required voltage. A diode is associated in arrangement at the positive

terminal of the PVA to stay away from invert currents going into the PVA. To decrease the swells a capacitor can be included later after the diode in parallel as the capacitor doesn't permit sudden difference in voltages dV/dt . The entire PVA module with interior square development is appeared in the fig. underneath

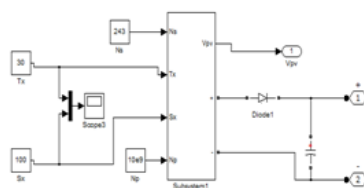


Fig. 9: Complete diagram of PVA

3 SIMULINK RESULTS AND CASE STUDY

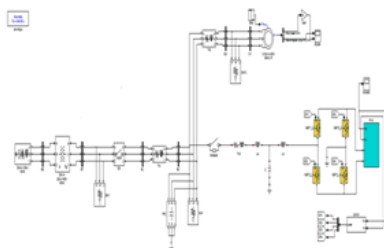


Fig. 12: Simulink Test system

Case Study 1 In this part, the investigative model-based recreation comes about are contrasted and the Matlab/SimPowerSystems display based reproduction comes about (to put it plainly, Sim-power). A solitary stage PV is associated with the period of the system at the purpose of basic coupling (PCC) appeared as in Fig. 1. the induction machine's mechanical torque was connected a stage change from 28 N.M to 23 N.M.

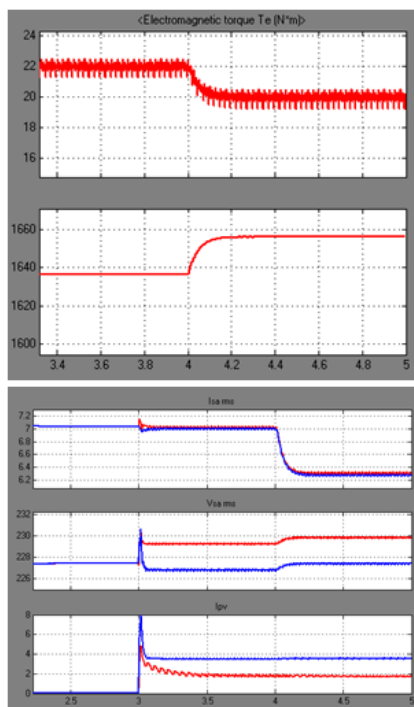


Fig. 13: Case I dynamic results

Case Study 2

In this part, the impact of PV irradiance change will be reenacted in both Matlab/Simulink and Matlab/SimPowersystems. the PV irradiance was set to 1000W/mt2 already. A slope change will be connected at to diminish the irradiance to 200W/mt2

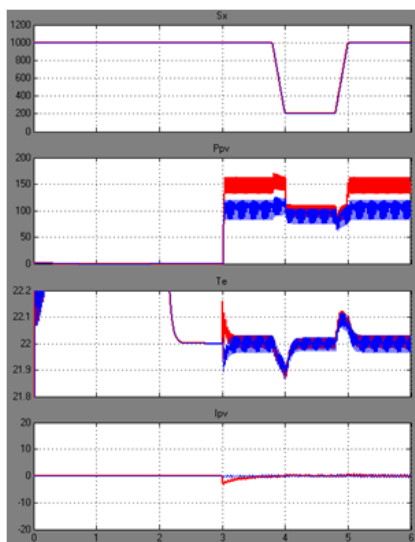


Fig. 14: Case II dynamic results

Case Study 3

The framework line length has been changed from 3 km to 15 km so as to watch its impact on flow. It merits saying that expanding the line length in excess of 15 km causes non-union of the general strategy for introduction.

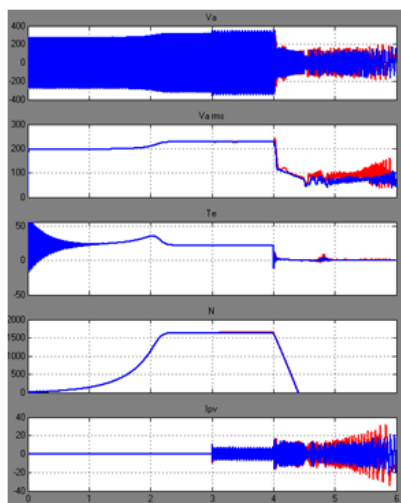


Fig. 15: Case III dynamic results

4 CONCLUSION

With the above outcomes in various dynamic cases the investigation of the test system is finished with dynamic aftereffects of Induction machine and Photo voltaic exhibit. The model is prepared to do quick time-space reenactment and little flag investigation. The model's exactness in catching time-space elements has been approved by Matlab/SimPowerSystems-based reproduction.

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